



Sensitivity and Structural Investigations on Shock Loaded and Quasi-Static Loaded KS22a HE

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"Material & Techniques for Reducing Sensitivity"

2004 Insensitive Munitions & Energetic Materials
Technology Symposium
Hilton - San Francisco, San Francisco, CA, USA
November 15 - 17, 2004

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Sensitivity and Structural Investigations on Shock Loaded and Quasi-Static Loaded KS22a

Outline:

- 1. Motivation**
Shock Loading of KS22a
- 2. TDW Gap Test**
Sensitivity Test
- 3. Shock Loading Mechanisms**
Static / Dynamic Loading of KS22a
- 4. Experimental Results**
Properties of Shock Loaded KS22a
- 5. Conclusion**
Summary

1. Motivation: Shock Loading of KS22a

Why Shock Loading of KS22a?

KS22a is a cost-effective, powerful but insensitive High Explosive for **penetrator applications**

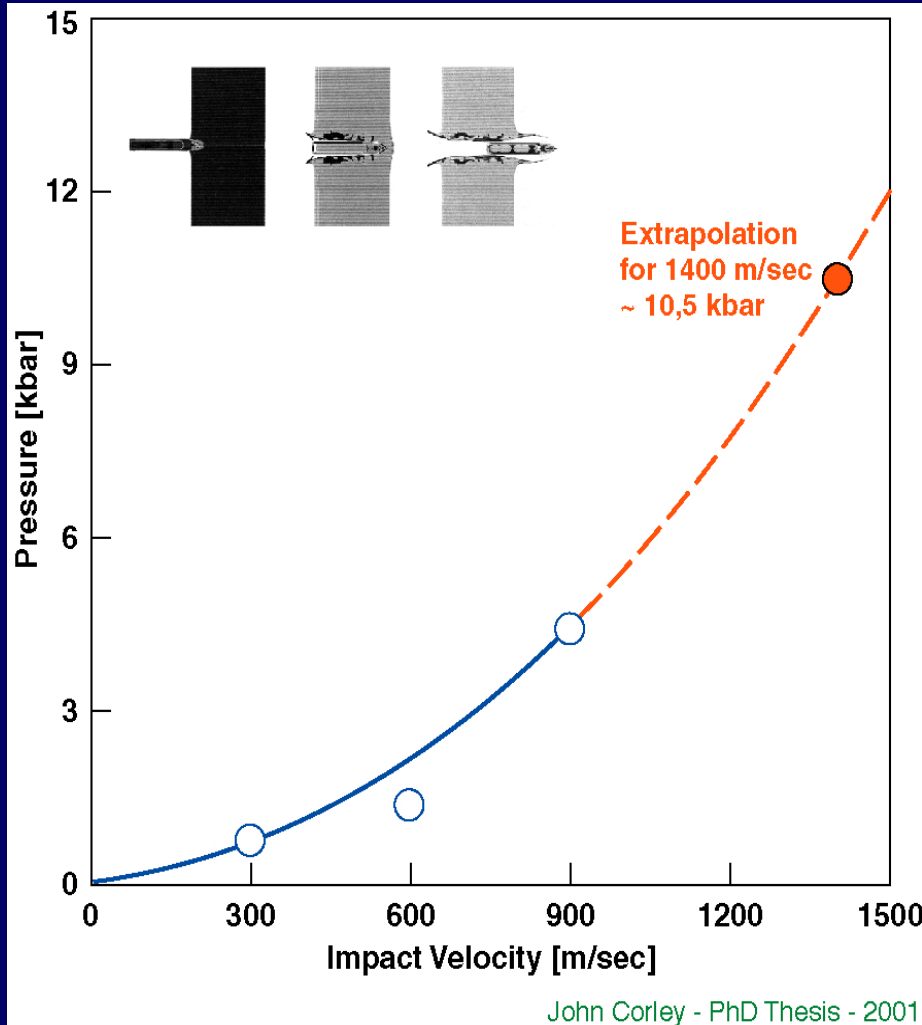
- It is RDX-based (67 % RDX)
- It is of the PBX-Type (15 % Plastic Binder)
- It is blast enhanced for improved performance in confined spaces (18 % Al)
 - It withstands high shock loads without degradation of ***performance***
 - **Question:** Will it withstand high shock loads without degradation of ***insensitivity*** as well?

German S/O Missile Taurus KEPD 350 *MEPHISTO Penetrator w/ KS22a*



Future Application with higher Shock Loads

Peak Pressure in Explosive Filler (Nose)



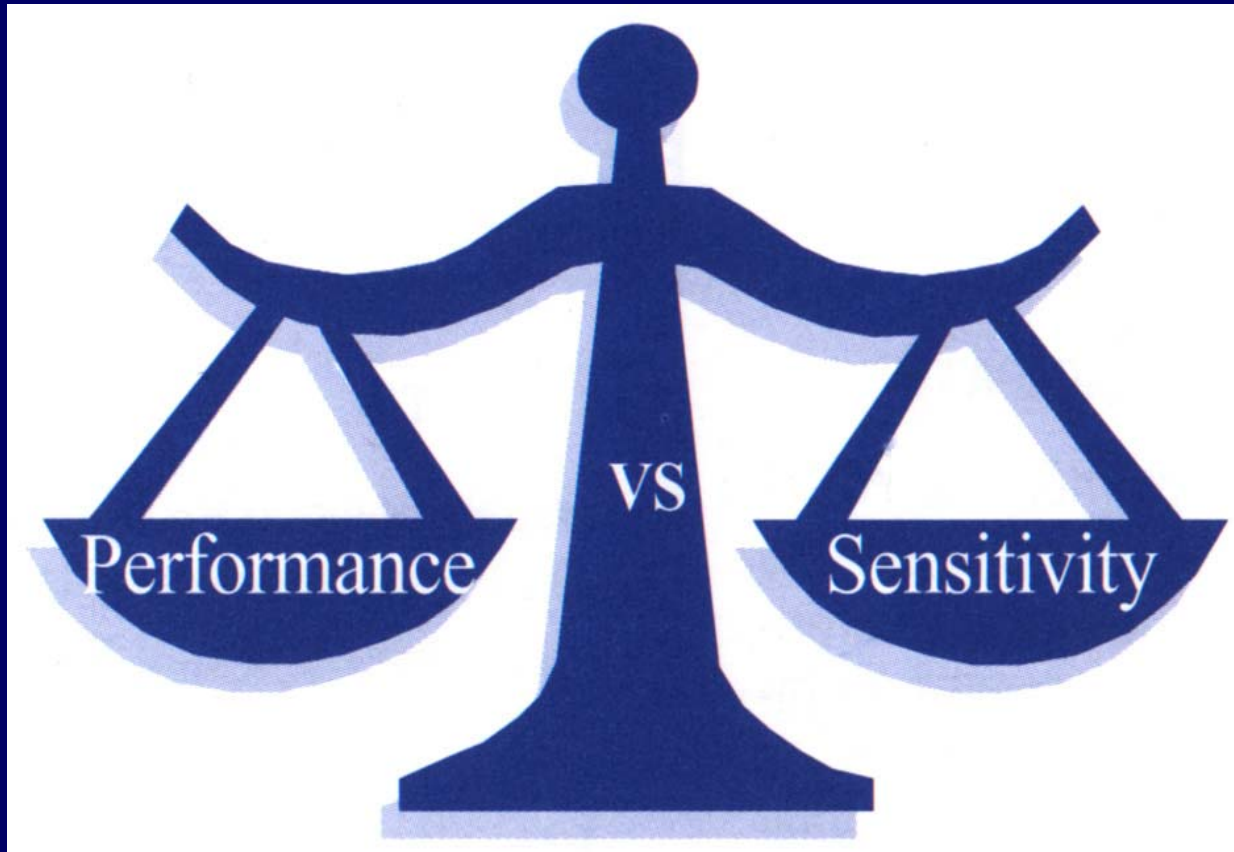
Simulation of Concrete Perforation (2 m, 35 MPa)

Question:

Will shock loads of several kbars influence the sensitivity of KS22a?

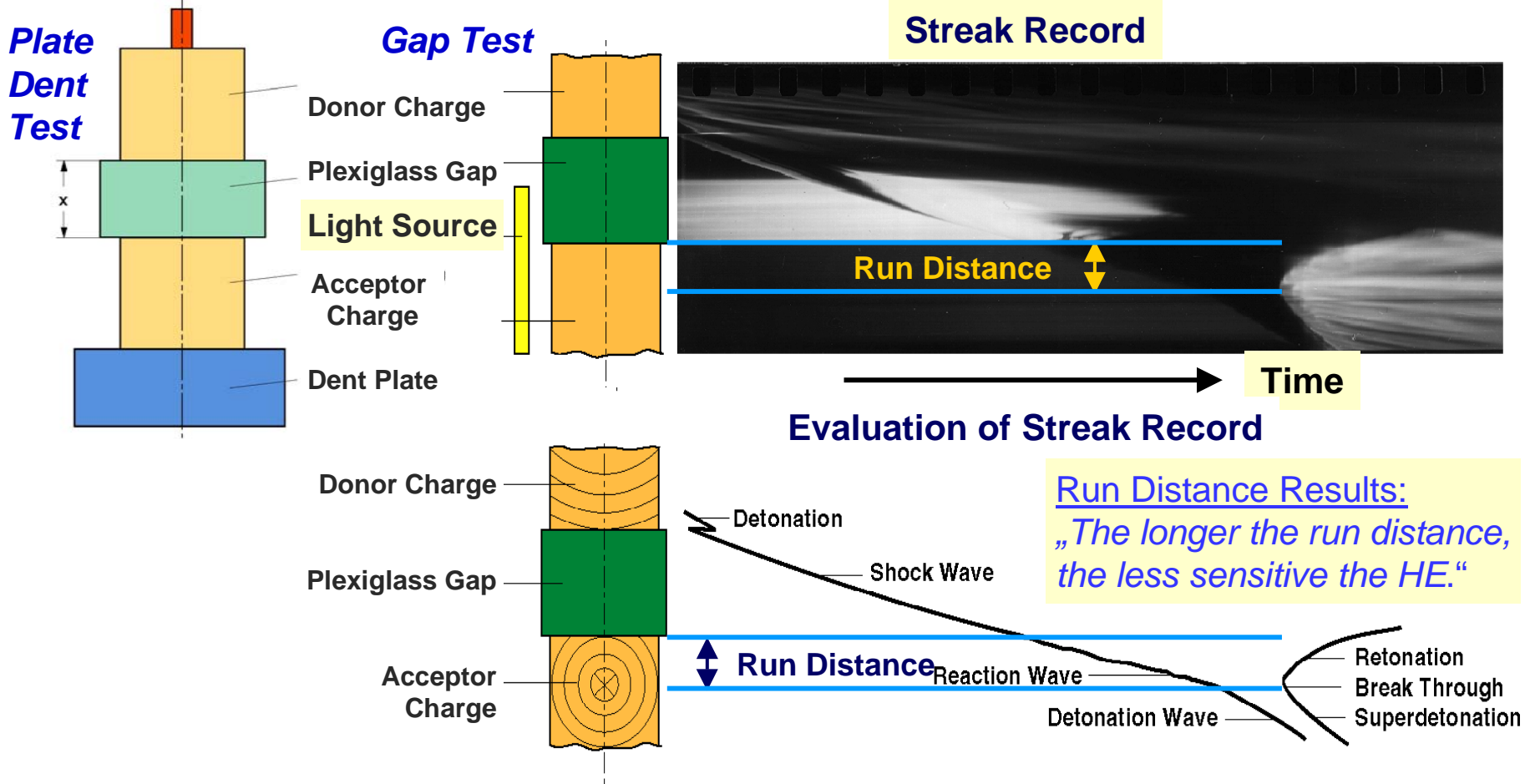
Balance between Performance vs. Sensitivity

Shock Loading of HE: Change in Sensitivity?



2. TDW Gap Test: Sensitivity Test

TDW Gap Test: Comparison between *Run Distance to Detonation and Plate Dent Depth*



3. Shock Loading Mechanisms

- Quasi-Static Loading: 200 ton Press
- Dynamic Loading: Cannon Firing (IMEMTS 2003)
- Dynamic Loading: Novel Shock Wave Apparatus

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Quasi-Static Loading

TDW's 200 ton Press



200 ton
Static Press

Downstroke
Ram



Static shock loading with
1 kbar and
4 kbar (axial loads)

Pressing
Confinement
58 mm



Lower
Ram

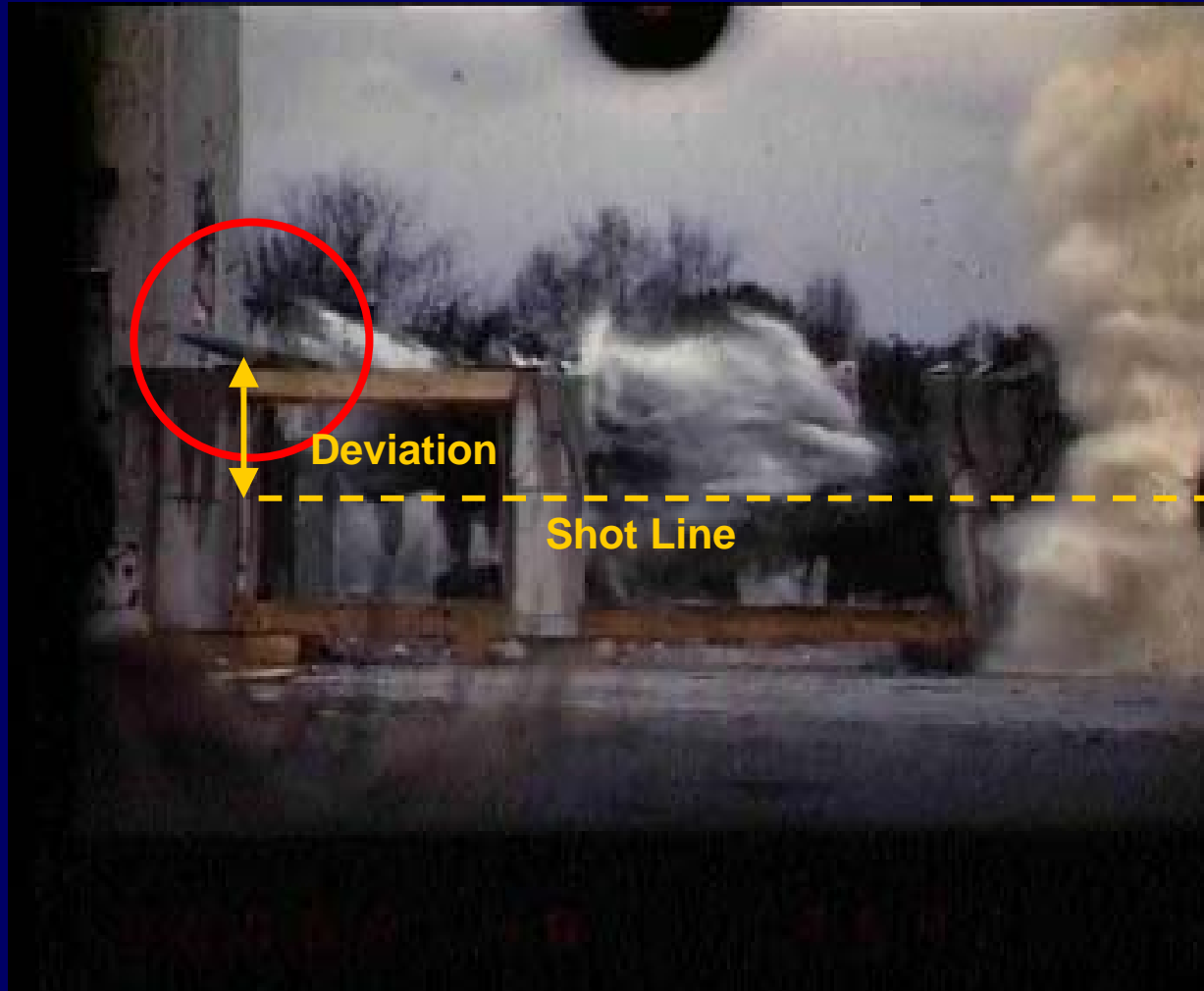


3. Shock Loading Mechanisms

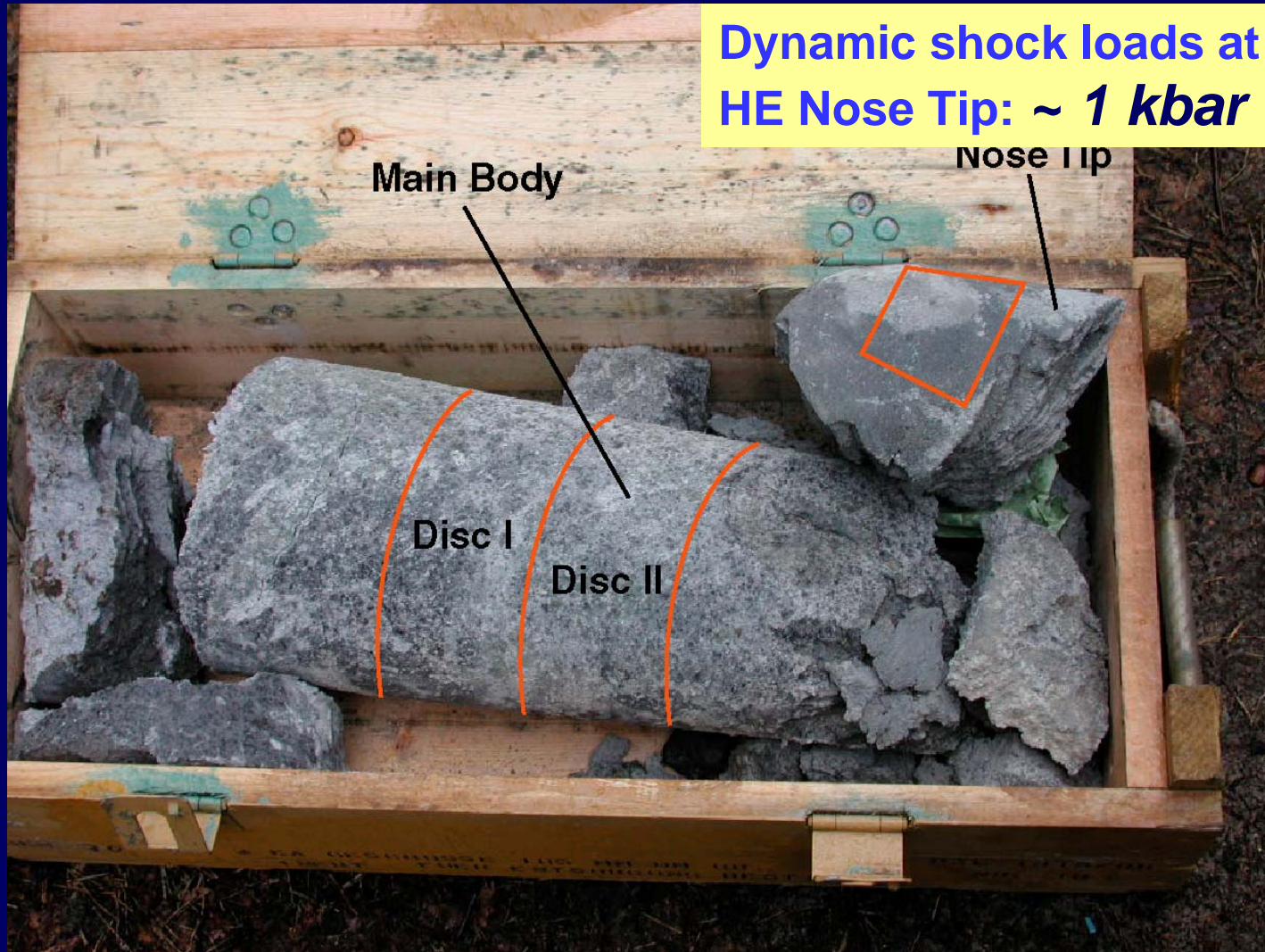
- Quasi-Static Loading: 200 ton Press
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- Dynamic Loading: Novel Shock Wave Apparatus

Dynamic Loading

Cannon Firing: Lateral Impact on Concrete Target



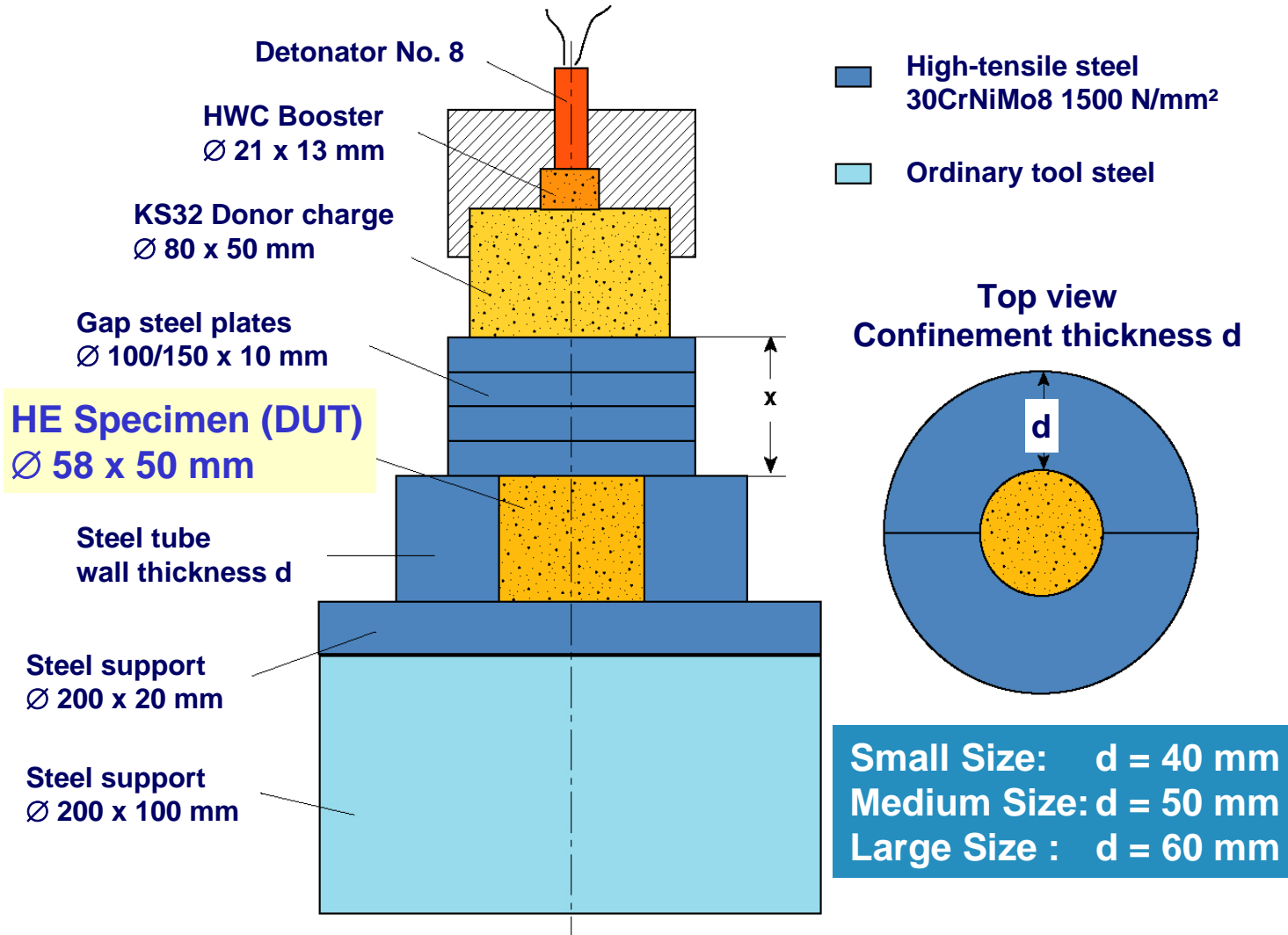
Pre-Shocked KS22a IHE Recovered after Test



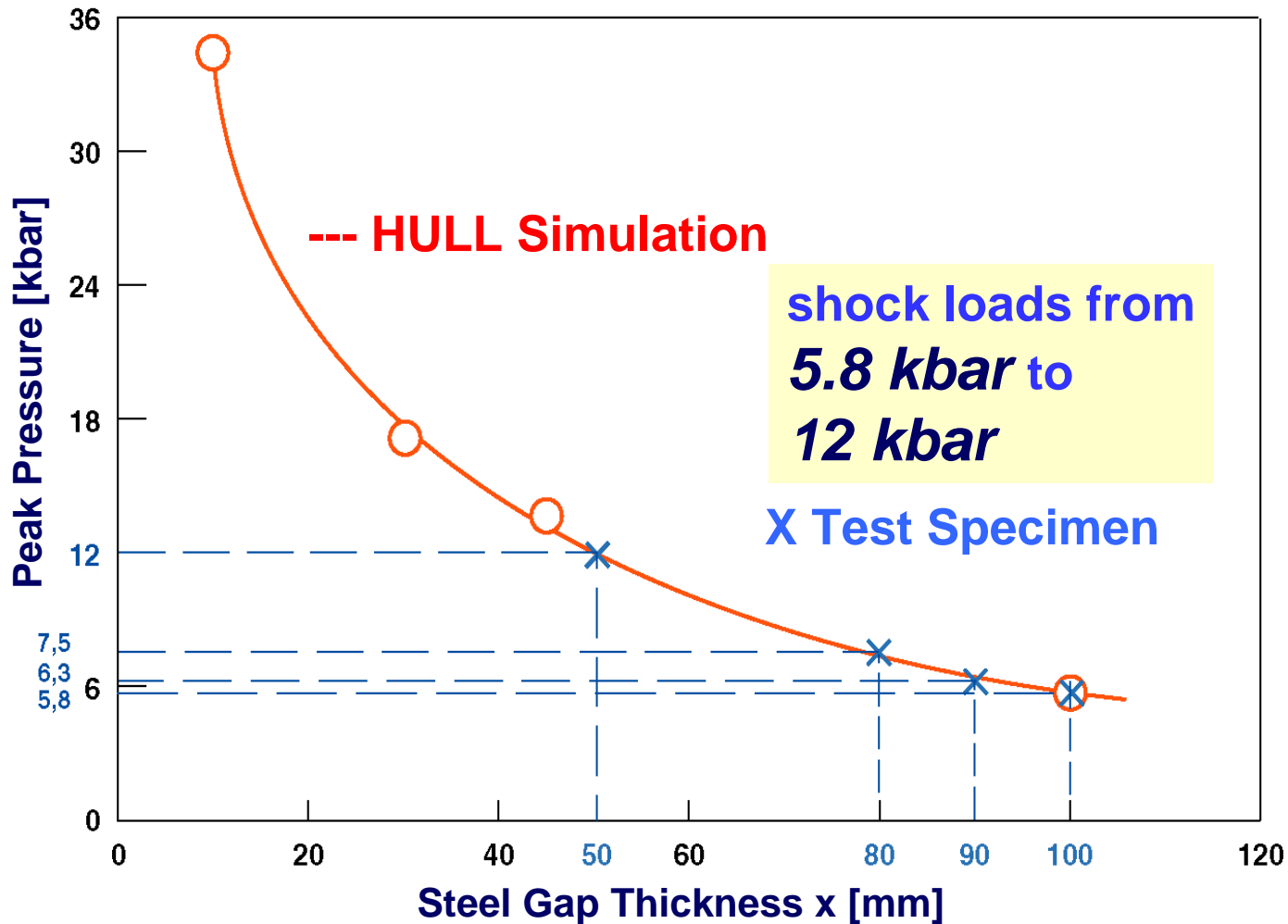
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Novel Shock Wave Apparatus: Three Sizes



Calibration: Peak Pressure vs Gap Thickness



Shock Wave Apparatus: Test with IHE KS22a Medium Size Variant



HWC Booster

KS32 Donor Charge

Steel Gap:
Thickness $x = 100$ mm

Casing of Specimen

Steel Support

Shock Wave Apparatus: Parts after Test

Medium Size Variant



Shock Wave Apparatus after Test



KS22a Specimen

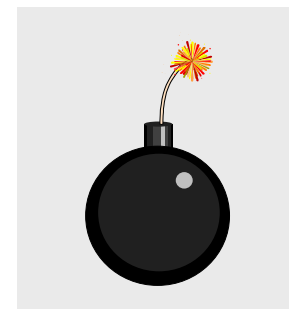
Mechanical Limit of Shock Wave Loading

KS22a Specimen after 7.5 kbar shock wave loading



Pre-Shocked KS22a Specimens

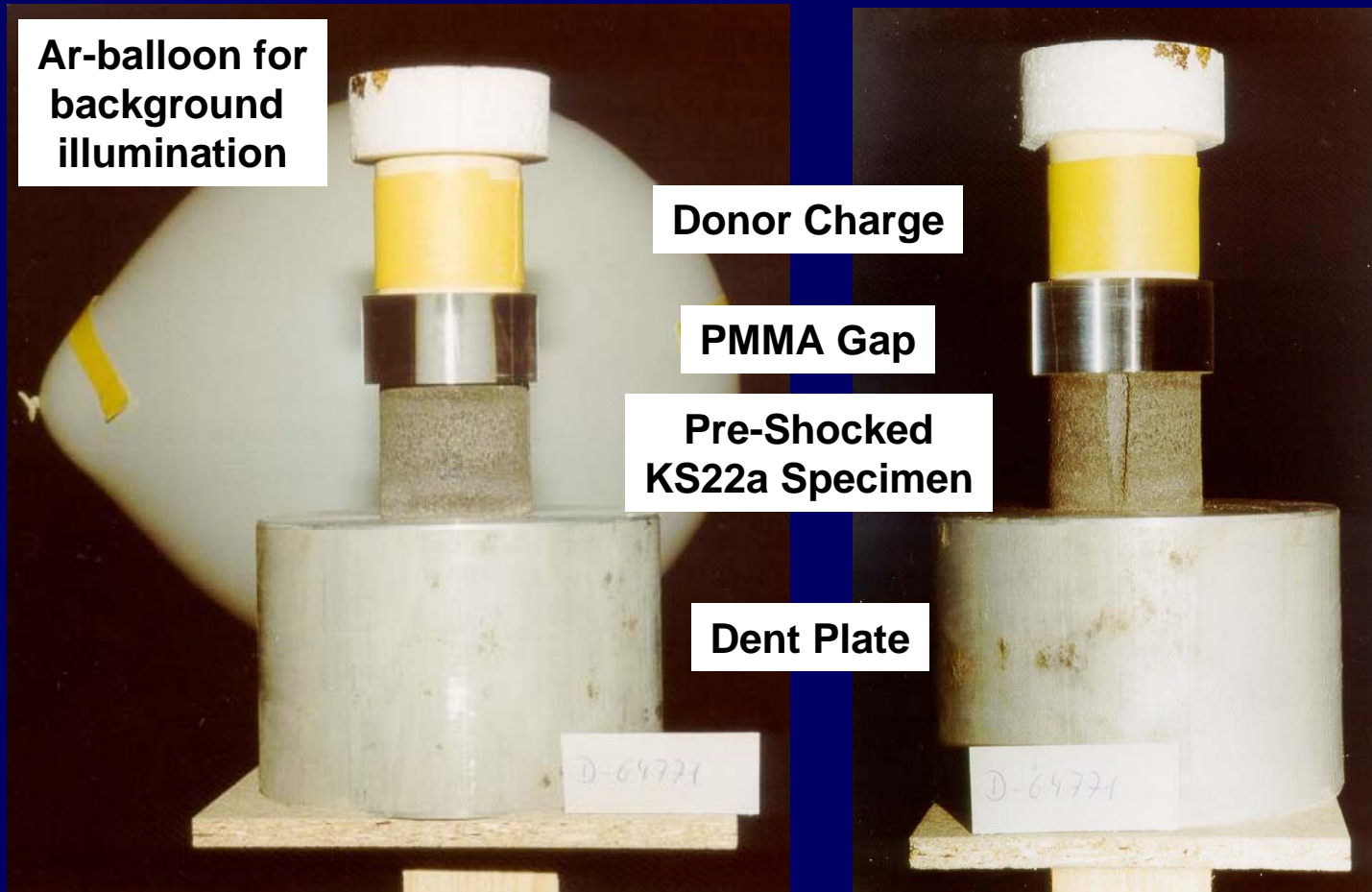
Mechanical Limit: ~ 7 kbar; Detonation: 12 kbar; (Bare: ~ 48 kbar)



Test No.	D-64788	D-64791	D-64790	D-64789
Gap thickness ↘	100 mm	90 mm	80 mm	50 mm
Shock load ↗	5.8 kbar	6.3 kbar	7.5 kbar	12 kbar
Sample property	intact	intact	cracks	detonated !
Gap Test suitability	possible	possible	not possible	/

Gap Test with Pre-Shocked KS22a Specimen

Experimental Set up



Front View

Side View

Test Result: KS22a Residual Parts after Gap Test

Mechanical Destruction due to Shock Damage



D-64771
5.8 kbar



D-64770
6.3 kbar

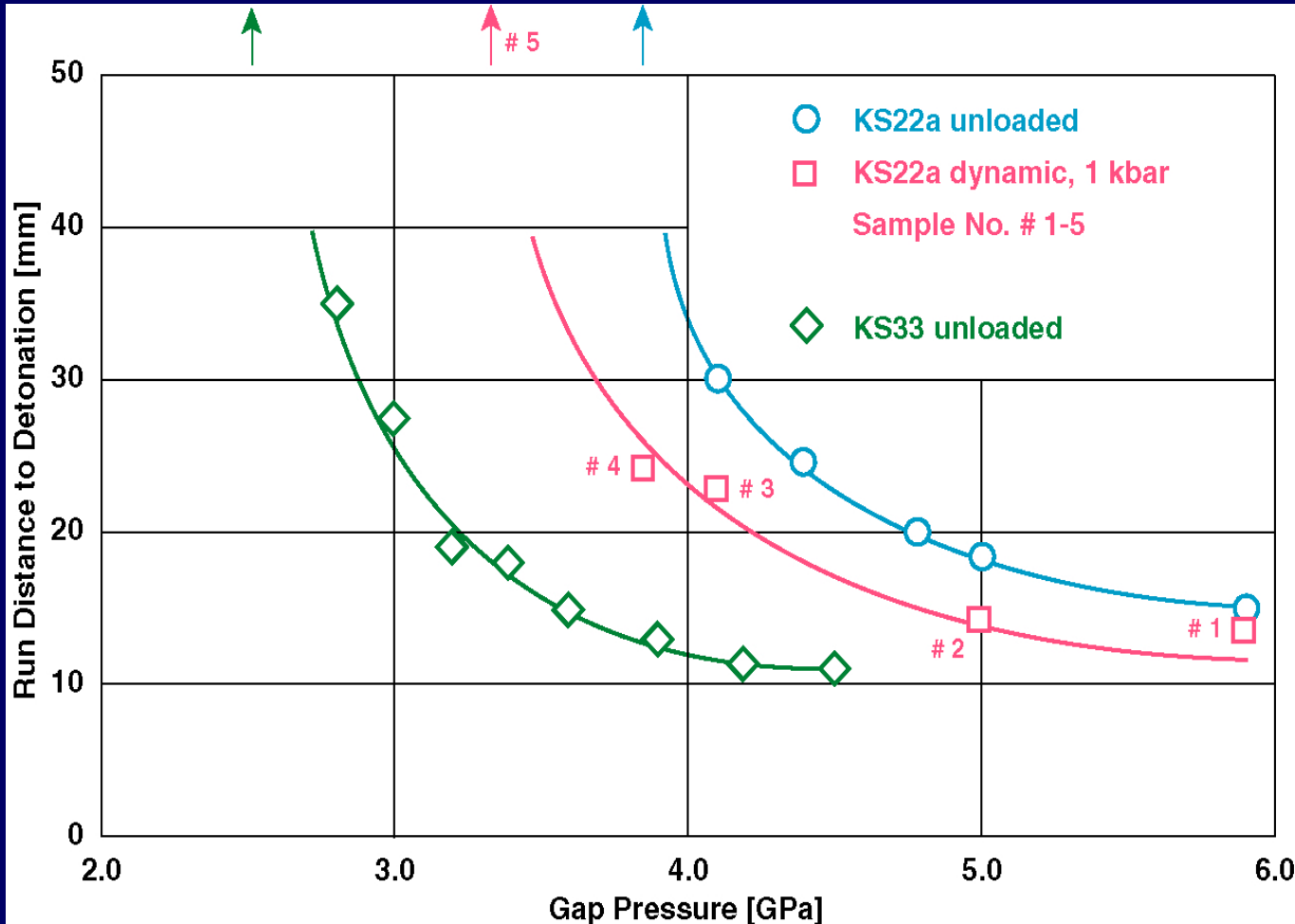
Reasons for Mechanical Destruction (*No Detonation*)

- Cracks, De-Bonding ... (reduced integrity) of specimen
- Starting of local reactions blew specimen apart
- No radial support in Bare Gap Test ...
- ... but *Detonation* within a penetrator casing to be expected

4. Experimental Results

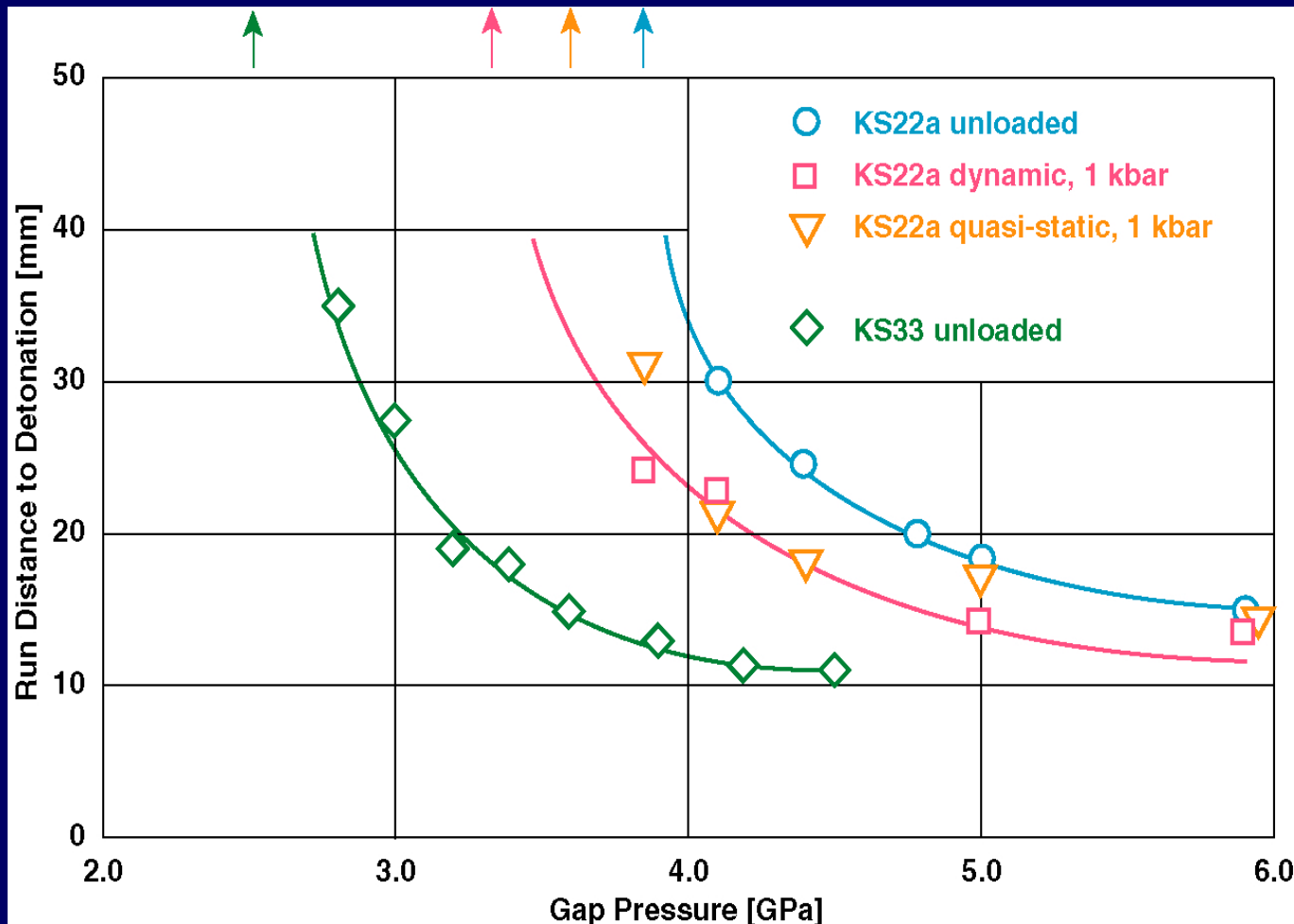
TDW Gap Test: Run Distance to Detonation

Reference: **KS33: HMX/PB 90/10** Density: 1.71 g/cc
KS22a: RDX/Al/PB 67/18/15 Density: 1.64 g/cc



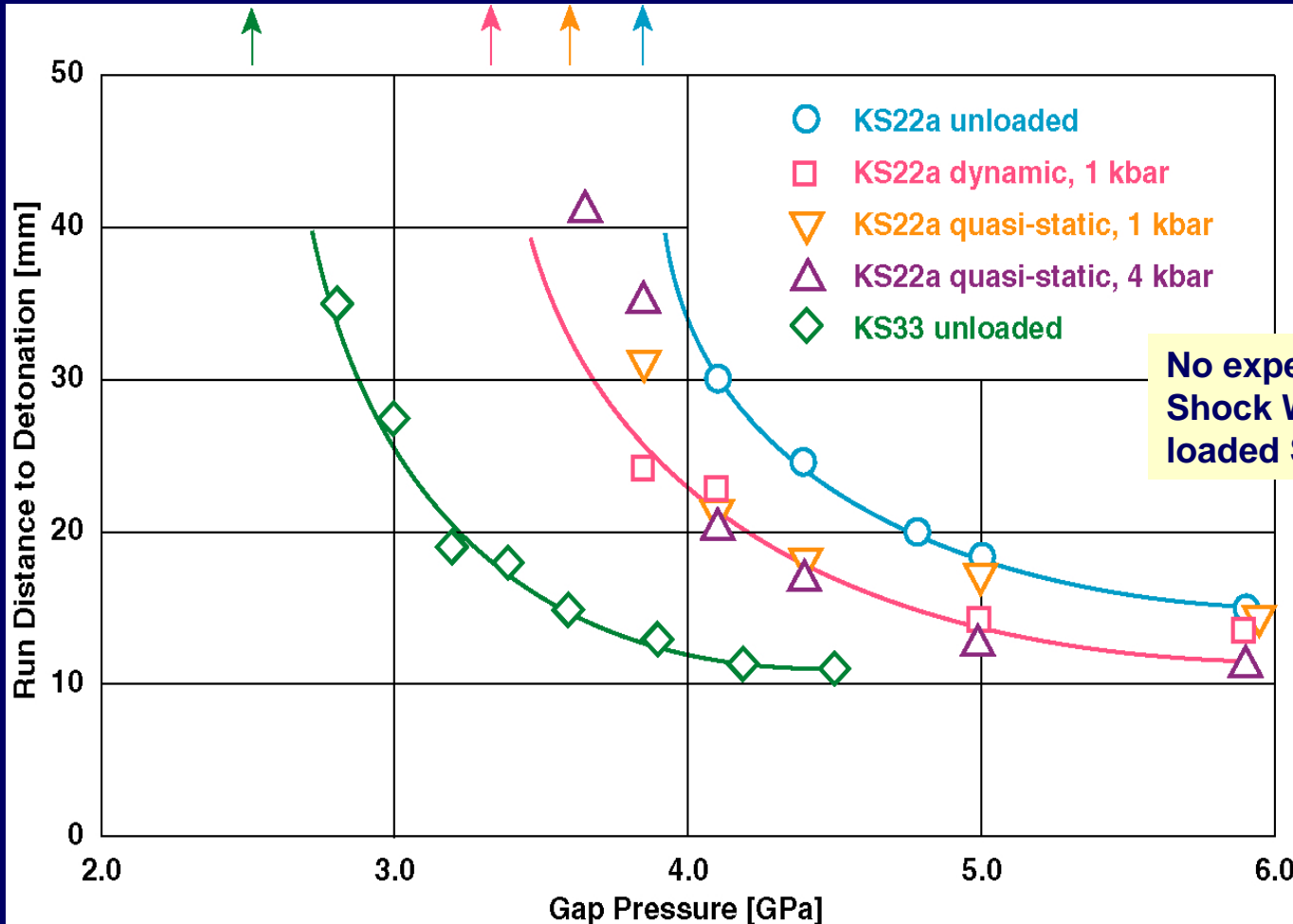
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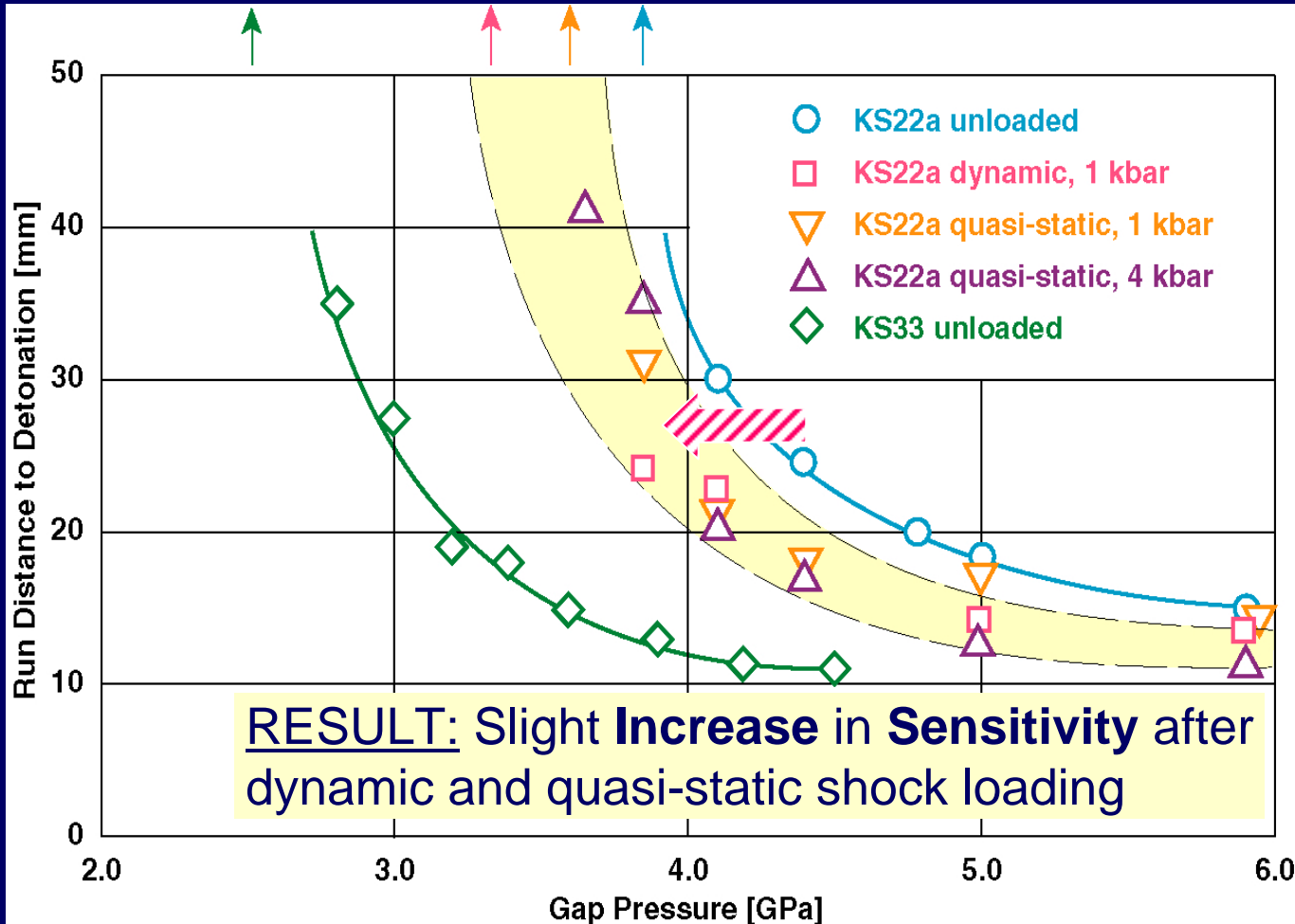
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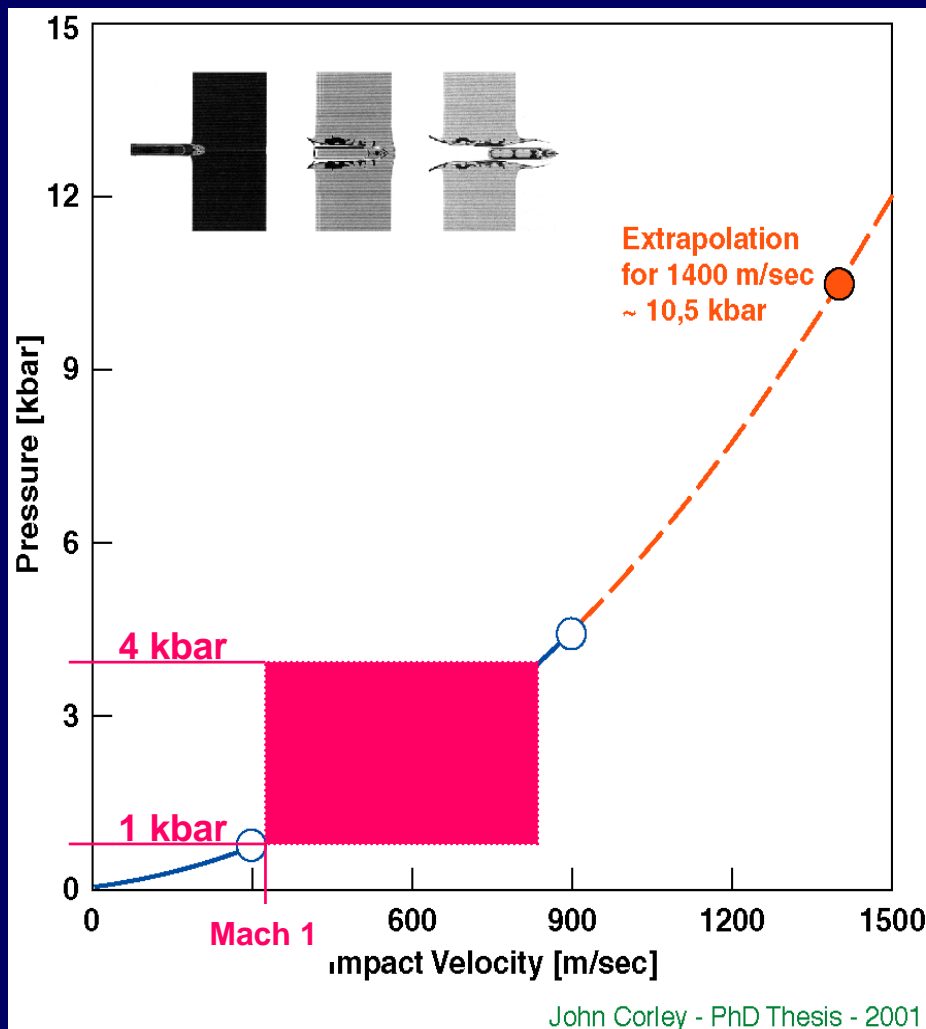
No experimental results of Shock Wave Apparatus loaded Specimen!

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Relevance of these Test Results for Real World Penetrator Applications



Shock loads of more than 1 kbar correspond to supersonic impacts with more than Mach 1.

Investigations on the Structure of KS22a

Structural Investigations by

- X-Ray Refraction
- X-Ray Diffraction
- Thermal Conductivity
- Scanning Electron Microscopy (SEM)

have been carried out by



Results: Possible Reasons for Changes of Sensitivity due to Static / Dynamic Loading

- Cracking of Grains
- Mechanical De-Bonding of Matrix / Grain Interfaces
- Local Reactions of RDX - Grains

Comparable Investigations by

A. Lefrancois et al. CEG (F): De-Bonding, Local Melting & Reaction
Dynamic Loading: RDX based HE, ~ 4 kbar, Scaled Penetrator

P. Peterson et al. LANL (USA): Cracking of HMX Crystals
Quasi-Static Loading: HMX based HE, 0.5 - 2 kbar, Press

have shown comparable results.

5. Conclusion

Observations and Conclusions

- Shock loading of HE in Supersonic Penetrators **is** an issue !
- Significant **reduction of initiation thresholds** due to radial confinement (**48 → 12 kbar**) observed
- **Changes in sensitivity** by quasi-static & dynamic shock loadings (Run Distance Tests) occurred
- This does not mean that KS22a is not suited for **Supersonic Penetrators** to be an **IM** !
- **Indications for defects** like de-bonding and grain fracture are likely the reasons for sensitivity changes

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patience!

Any Questions?